# An investigation the effects of generalized skew coefficient (Third moment) on instantaneous annual maximum discharges.

(Case study: Dez basin in south western of Iran)

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#### 1.Abstract

One of the methods of reduce flood hazard is correct estimation discharge designing of water structures, because without computation of estimated discharge water structures is destroy by flood occurrence and increase flood hazard power. Use of data in gauging stations in the area is the best method for estimation discharge flood design. Also computation of generalized coefficient skew of measurement data decrease estimated error and water structures dimensions improve designing in the basin without gauging stations or with short data. The study is located in 47 degree and 39 minute to 50 degree and 21 minute in eastern length and 31 degree and 15 minute to 34 degree and 33 minute in northern latitude. We selected 24 gauging stations. Then, the test of outlier was conducted by using statistical parameters of peak flow in the hydrometric stations, and it was determined that there are no outlier points among data. So completing and lengthening for common statistical period performed. Then statistical distribution of aforementioned data was fitted. Using griding method, the centroid of high area of each hydrometric station was determined generalized skew coefficients of points then were computed using the unbiased skew coefficient, the weight coefficient of data and the distance of each hydrometric gauge from centroid of sub-basin. Spline (Smooth plate Line) method was applied to generalize the skew with the mean square error of %34. The results show that the range of percentage of differences between unbiased and generalized skew are from 58% to 137%. The observed data have been fitted well with the normal distribution. using this method results less differences between observed and estimated values of peak discharges as where generalized skew were used, the differences of peaks for return periods of 2, 100 and 1000 years, were %12, %77 and %180 respectively. It can be concluded that the fitness of selected probability distribution with the data is quite best using the generalized skew in estimation of peak discharge.

Keyword: Generalized coefficient, Hydrometric, station skew, Instantaneous maximum discharge, Dez basin.

#### 2.Introduction

The analysis of peak flow is fund a mental to the design of drainage facilities. Errors in the estimates will result in a structure that is either undersized and causes more drainage problems or oversized and costs mor than necessary.

2. Flood frequency analysis is an essential of extreme floods (i.e.Greater than a 1000 year flood)

All regionalization methods implicitly or explicitly make assumptions about the regional distribution of annual floods. One of the most common regionalization methods utilizes normalized annual flood series, that is, flood series that have been standardized by one more at-site statistics.

Flood frequency curve for individual gaging station were developed following the guidelines described in Bulletin 17B, Interagency advisory committee on water data (1982). A log-pearson type three distribution function was used to fit annual peak discharges to log-probability curves (Giese and Franklin 1996). Bulletin 17Brecommends the use of generalized skew coefficients developed from detailed studies using pooled information from nearby long-term stations instead of generalized skew coefficients taken from the nationwide mapor plotting station skew coefficient on a map and drawing lines of equal values. (Williams-sether 1992)

Naghavi ,Babak and Fang Xin yu (1991) provided generalized skew map for Louisiana streams, Misssissippi,Arkansas and Texas with 200r more years of annual flood recorders and show that mean square error for Louisiana generalized skew map is 16 percent Less than generalized skew map recommended by the u.s Water Resources Council.

Hodgkins and Martin (2003)

Estimated of peak flow are given for 222 gaging stations in Kentucky .In the development of the peak flow estimated at gaging stations, a new generalized skew coefficient was calculated for the state. This single statewide value of 0.011 (with a standard error of prediction of 0.520)

Is more appropriate for Kentuky than the national skew isoline map in Bulletin 17B of the Interagency Advisory Committee on Water Data.

# 3.Materials and methods

# 3.1. **LOCATION**

Watershed Dez located in the south West of IRAN (Figure 1)



Figure 1 Location of Dez basin in map of IRAN

# 3.2. Characteristic of gaging stations

in this study selected 24 station that shown their characteristic in the table 1.

Table1 characteristics of gaging station in Dez basin

| Table1 characteristics of gaging station in Dez basin |                 |                     |               |              |                     |                   |  |  |  |
|---|-----------------|---------------------|---------------|--------------|---------------------|-------------------|--|--|--|
| Elevation (m)   | Latitude (ddmm) | Longitude<br>(ddmm) | Area $(km^2)$ | Station code | Station name        | River name        |  |  |  |
| 1520  | 33-39           | 49-01               | 973           | 21-255       | Do khaharan         | Tireh             |  |  |  |
| 1980  | 33-55           | 48-36               | 65            | 21-257       | Vanaee              | Sarab sefid       |  |  |  |
| 2000  | 33-54           | 48-35               | 60            | 21-259       | Vanaee              | Gale rud          |  |  |  |
| 1490  | 33-47           | 48-48               | 1000          | 21-261       | Rahim abad          | Silakhor          |  |  |  |
| 1540  | 33-44           | 48-46               | 223           | 21-263       | Boz azna            | Absardeh          |  |  |  |
| 1600  | 33-42           | 48-58               | 120           | 21-265       | Biatun              | Biatun            |  |  |  |
| 1450  | 33-29           | 49-04               | 3400          | 21-267       | Do rud              | Tireh             |  |  |  |
| 1830  | 33-24           | 49-24               | 2010          | 21-271       | Cham zaman          | Azna              |  |  |  |
| 1930  | 33-19           | 49-26               | 35            | 21-273       | Kamandan            | Kamandan          |  |  |  |
| 1890  | 33-23           | 49-23               | 36            | 21-275       | Dare takht          | Dare takht        |  |  |  |
| 1800  | 33-29           | 49-22               | 2185          | 21-277       | Dare takht          | Mar bareh         |  |  |  |
| 1450  | 33-29           | 49-05               | 2655          | 21-279       | Do rud              | Mar bareh         |  |  |  |
| 1290  | 33-13           | 48-59               | 345           | 21-281       | Cham chit           | Ab sabzeh         |  |  |  |
| 1000  | 33-14           | 48-54               | 158           | 21-283       | Sepid dasht         | Vask              |  |  |  |
| 970   | 33-13           | 48-53               | 7174          | 21-285       | Sepid dasht         | Sezar             |  |  |  |
| 970   | 33-13           | 48-53               | 680           | 21-287       | Sepid dasht         | Zaz               |  |  |  |
| 770   | 33-08           | 48-38               | 336           | 21-289       | Keshvar             | Sorkhab           |  |  |  |
| 600   | 32-56           | 48-45               | 9410          | 21-291       | Tang panj           | Sezar             |  |  |  |
| 540   | 32-56           | 48-46               | 6432          | 21-293       | Tang panj           | Bakhtiari         |  |  |  |
| 480   | 32-49           | 48-46               | 16213         | 21-295       | Tale zang           | Dez               |  |  |  |
| 2000  | 33-08           | 49-41               | 438           | 21-400       | Kazem abad          | Kakolestan        |  |  |  |
| 2355  | 32-51           | 50-01               | 58254         | 21-402       | Zard fahrami        | Vehargan          |  |  |  |
| 2000  | 33-00           | 49-48               | 744           | 21–457       | Cheshme<br>langan   | Cheshme<br>langan |  |  |  |
| 1850  | 33-04           | 49-39               | 414           | 21-968       | Gholian<br>(sekane) | Gholian           |  |  |  |

#### 3.3. Determination of outlier

For determination of outlier used of bellow equation and there are no outlier

$$(1) X_{HL} = \overline{X} \pm k_N S$$

There:

 $X_H$ = up outlier threshold;

 $X_L$ = Down outlier threshold;

Mean of data; X =

S= Standard deviation; and

K<sub>N</sub>= Frequency coefficient of outlier.

#### 3.4. Skew Coefficient of Station

The station coefficient is computed as follows:

$$G_{s} = \frac{N}{(N-1)(N-2)S^{3}} \sum_{i=1}^{N} (X_{i} - \overline{X})^{3}$$
 (2)

Where:

G<sub>x</sub>=stations skew coefficient;

X<sub>i</sub>=stations log-transformed annual peak discharge for yeari;

x = stations log-transformed mean of annual peak discharges;

S=stations log-transformed standard deviation of annual peak discharges;

N=station number of years of peak discharge record.

Many studies have shown that the stations skew coefficient is a biased estimator of the populations skew coefficient.

A bias –correction equation based on record length (years) is presented by Tasker and stedinger (1986) as:

$$C_b = (1 + \frac{6}{N}) \tag{3}$$

Where:

C<sub>b</sub>=stations bias-correction factor; And

N=stations number of year of peak-discharge record.

The station skew coefficient (G<sub>s</sub>) for each of the 24 stations (sample) used in this study was multiplied by the bias-correction factor to obtain and unbiased value (Table 2)

#### 3.5. Generalized and weighting of skew coefficient

In this study generalized skew coefficients are estimated from mapping . The estimating technique referred to above assume that the skew coefficient for each station have equal accuracy. Many investigation developed have equation to estimate the variance of stations skew coefficient  $(V_s)$  to vary with record Length (N) and corrected for bias and defined as:

$$V_{a} = \frac{6N(N-1)[1+(6/N)]^{2}}{(N-2)(N+1)(N+3)}$$
(4)

A stations skew coefficient is weighted in verse proportion to the estimated stations

variance (v<sub>s</sub>); (Lumia and Bavesky 2000) there for, The weight given for each stations skew coefficient is;

$$W = \frac{1}{V_s} \tag{5}$$

Where:

W= is the weight given to the stations unbiased skew coefficient and  $V_s$  is as defined previously.

The variance of gaging station skew coefficient and weight given to the station unbiased skew coefficient calculated for each of the 24 stations (table 2)

Table 2 Skew coefficient and weighted coefficient of peak flow data in Dez basin

| W     | $G_{s}$ | Station code | Station name        | River<br>name     |  |
|-------|---------|--------------|---------------------|-------------------|--|
| 2.560 | -0.018  | 21-255       | Do khaharan         | Tireh             |  |
| 1.516 | -0.345  | 21-257       | Vanaee              | Sarab sefid       |  |
| 2.256 | 0.122   | 21-259       | Vanaee              | Gale rud          |  |
| 2.256 | -0.343  | 21-261       | Rahim abad          | Silakhor          |  |
| 1.516 | 0.260   | 21-263       | Boz azna            | Absardeh          |  |
| 1.232 | 0.657   | 21-265       | Biatun              | Biatun            |  |
| 4.128 | 0.314   | 21-267       | Do rud              | Tireh             |  |
| 2.715 | -0.262  | 21-271       | Cham zaman          | Azna              |  |
| 2.256 | 0.263   | 21–273       | Kamandan            | Kamandan          |  |
| 2.256 | 0.273   | 21-275       | Dare takht          | Dare takht        |  |
| 3.338 | 0.004   | 21-277       | Dare takht          | Mar bareh         |  |
| 1.956 | 0.750   | 21-279       | Do rud              | Mar bareh         |  |
| 4.128 | -0.03   | 21-281       | Cham chit           | Ab sabzeh         |  |
| 4.128 | -0.164  | 21–285       | Sepid dasht         | Sezar             |  |
| 3.025 | 0.075   | 21-287       | Sepid dasht         | Zaz               |  |
| 2.408 | 0.433   | 21-289       | Keshvar             | Sorkhab           |  |
| 2.715 | 0.299   | 21-291       | Tang panj           | Sezar             |  |
| 3.338 | 0.681   | 21-293       | Tang panj           | Bakhtiari         |  |
| 4.447 | -0.853  | 21-295       | Tale zang           | Dez               |  |
| 1.808 | -0.351  | 21-400       | Kazem abad          | Kakolestan        |  |
| 1.661 | -0.411  | 21-402       | Zard fahrami        | Vehargan          |  |
| 1.661 | 0.96    | 21-457       | Cheshme<br>langan   | Cheshme<br>langan |  |
| 1.808 | 0.535   | 21-968       | Gholian<br>(sekane) | Gholian           |  |

#### 4. Conclusion

### 4.1. Map of skew coefficient

For mapping of skew coefficients Dez watershed with an equally spaced grid was plotted along with station skew coefficients for each study site of gaging station and geographic information systems (GIS) software was used to compute and unbiased

skew coefficient for each node of the grid. The skew coefficient for each calculated from the following equations; (Lumia and Bavesky 2000)

(6) 
$$Z_i = \frac{\sum_{i=1}^n G_{sj}(W_j)(\frac{1}{d_j})}{\sum_{i=1}^n (W_j)(\frac{1}{d_j})}$$

#### Where:

Z<sub>i</sub>= estimated skew coefficient at grid node;

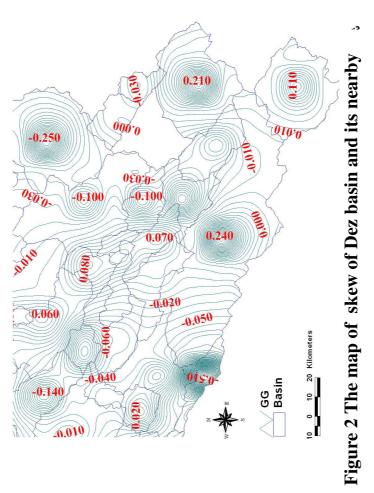
G<sub>sj</sub>= unbiased skew coefficient of station j;

n= number of stations selected to estimated Z<sub>i</sub>;

 $d_j$ = distance from the grid node to centroid of drainage basin whose records define  $G_{si}$ 

 $W_i$ = weight given to  $G_s$  at station j.

By using equations 2 and 3 bias and skew coefficient for selected stations were computed than unbiased skew coefficient was computed for each grid node by the weighting procedure of equation 6 and Isoline skew coefficient were fitted through the grid node coefficients by an automated geographic information systems (GIS) technique. In Figure 2 generalized unbiased skew coefficient map is given.



- 4.2. Determination of best calculation method of generalized skew coefficient .
- In this study generalized skew coefficient calculated by use of Isoline skew on the map . For evaluation of generalized skew coefficient accuracy compared mean square errors of four contour map to evaluate other methods to identify which one would provide the most accurate generalized skew coefficient . The methods evaluated were :
- (1) Calculation of unbiased skew coefficient for each of grid node by TPSS, (2) The arithmetic unweighted means of the unbiased skew coefficient for each of grid node by TPSS, (3) calculation of inverse distance weight and unbiased skew coefficient for each of grid node, and (4) calculation of unbiased skew coefficient and inverse distance weight for each of grid node. Mean square errors (MSE) for each of the four methods of predicting generalized skew coefficients were computed for all regions and are based on observed and predicted skew coefficients at gaging stations. Generally, smallest (MSE) resulted from the first method (34%). The results are included in table 3, which shows generalized skew coefficient for each of the methods.

Table3 calculation methods of generalized skew of peak flow in Dez basin

| G <sub>G</sub><br>by<br>IDW or mean | G <sub>G</sub><br>by<br>IDW | G <sub>G</sub> by TPSS or mean | G <sub>G</sub> by TPSS <sup>1</sup> | $G_{s}$ | N  | Station code |
|-------------------------------------|-----------------------------|--------------------------------|-------------------------------------|---------|----|--------------|
| -0.016                              | 0.036                       | 0.002                          | 0.051                               | -0.018  | 22 | 21-255       |
| -0.001                              | 0.013                       | -0.005                         | 0.005                               | -0.345  | 15 | 21-257       |
| 0.001                               | -0.009                      | -0.008                         | -0.005                              | 0.122   | 20 | 21-259       |
| 0.010                               | 0.014                       | 0.009                          | -0.009                              | -0.343  | 20 | 21-261       |
| 0.016                               | -0.021                      | 0.025                          | -0.019                              | 0.260   | 15 | 21-263       |
| -0.013                              | 0.037                       | 0.003                          | 0.056                               | 0.657   | 13 | 21-265       |
| -0.015                              | -0.017                      | -0.016                         | -0.009                              | 0.314   | 32 | 21-267       |
| -0.058                              | 0.039                       | -0.080                         | 0.048                               | -0.262  | 23 | 21-271       |
| -0.043                              | 0.053                       | -0.061                         | 0.063                               | 0.263   | 20 | 21-273       |
| -0.033                              | 0.051                       | -0.034                         | 0.053                               | 0.273   | 20 | 21-275       |
| 0.040                               | 0.056                       | -0.060                         | 0.063                               | 0.004   | 27 | 21-277       |
| -0.016                              | -0.015                      | -0.017                         | -0.009                              | 0.750   | 18 | 21-279       |
| 0.002                               | -0.059                      | 0.015                          | -0.064                              | -0.030  | 32 | 21-281       |
| -0.007                              | -0.050                      | 0.001                          | -0.052                              | -0.164  | 32 | 21-285       |
| -0.004                              | -0.047                      | -0.001                         | -0.049                              | 0.075   | 25 | 21-287       |
| -0.019                              | -0.037                      | -0.025                         | -0.019                              | 0.433   | 21 | 21-289       |
| 0.016                               | -0.316                      | 0.022                          | -0.388                              | 0.299   | 23 | 21-291       |
| 0.007                               | -0.192                      | 0.011                          | -0.260                              | 0.681   | 27 | 21-293       |
| 0.007                               | -0.191                      | 0.016                          | -0.340                              | -0.853  | 34 | 21-295       |
| -0.002                              | -0.060                      | 0.002                          | -0.064                              | -0.351  | 17 | 21-400       |
| 0.002                               | -0.075                      | 0.010                          | -0.085                              | -0.411  | 16 | 21-402       |
| -0.009                              | -0.018                      | 0.001                          | -0.019                              | -0.960  | 16 | 21-457       |
| 0.021                               | -0.135                      | 0.028                          | -0.143                              | 0.535   | 17 | 21-968       |

# 4.3. Estimation of peak flow by using generalized skew

By using this method results less differences between observed and estimated values of peak discharges as where generalized skew were used, the differences of peaks for return periods of 2, 100 and 1000 years, were %12, %77 and %180 respectively. It can be concluded that the fitness of selected probability distribution with the data is quite best using the generalized skew in estimation of peak discharge (Table 4).

Table 4 Peak flow  $\binom{m^3}{s}$  by using unbiased skew coefficient for recurrence

interval, in year

| 1000    | 500     | 200     | 100    | 50     | 25     | 20      | 10      | 5      | 2      | Q <sub>t</sub> S.code |
|---------|---------|---------|--------|--------|--------|---------|---------|--------|--------|-----------------------|
| 975.05  | 804.50  | 611.35  | 487.22 | 380.06 | 288.20 | 261.62  | 187.58  | 125.25 | 57.7   | 21-255                |
| 33.49   | 30.98   | 27.60   | 25     | 22.36  | 19.65  | 18.76   | 15.92   | 12.93  | 8.40   | 21-257                |
| 45.56   | 40.54   | 34.37   | 30.04  | 25.96  | 22.12  | 20.92   | 17.32   | 13.83  | 9.09   | 21-259                |
| 543.58  | 443.47  | 333.67  | 265.17 | 207.35 | 158.71 | 144. 79 | 106.26  | 73.95  | 38.35  | 21-263                |
| 2721.12 | 1577.50 | 749.36  | 417.14 | 226.35 | 118.71 | 95.55   | 46.84   | 21.07  | 5.52   | 21-265                |
| 126.03  | 102.26  | 76.35   | 60.31  | 46.85  | 35.61  | 32.41   | 23.60   | 16.27  | 8.30   | 21–273                |
| 63.81   | 52.86   | 40.64   | 32.88  | 26.20  | 20.48  | 18.81   | 14.16   | 10.15  | 5.56   | 21–275                |
| 338.37  | 302.29  | 257.30  | 225.17 | 194.56 | 165.30 | 156.14  | 128.31  | 101.07 | 63.85  | 21-281                |
| 1129.45 | 984.27  | 809.94  | 690.32 | 580.35 | 479.16 | 448. 29 | 357.14  | 271.92 | 162.83 | 21-287                |
| 1560.07 | 1296.38 | 1001.84 | 816.12 | 656    | 520.64 | 481.04  | 369.60  | 273.10 | 160.82 | 21-289                |
| 361.45  | 320.56  | 268.42  | 230.53 | 194.04 | 159.01 | 148.04  | 114.97  | 83.30  | 42.78  | 21-400                |
| 390.55  | 359.64  | 318.07  | 286.03 | 253.41 | 220.09 | 209.17  | 174. 53 | 138.16 | 84.80  | 21–402                |
| 1005.13 | 808.93  | 600.21  | 473.77 | 369.46 | 283.54 | 259.25  | 192.76  | 137.69 | 77.29  | 21-968                |

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